

## In-situ Fabricated TiB<sub>2</sub> Particle-whisker Synergistically Toughened Ti(C, N)-based Ceramic Cutting Tool Material

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**Abstract:** The mechanical properties of ceramic cutting tool materials can be modified by introducing proper content of nanoparticles or whiskers. However, the process of adding whiskers or nanoparticles has the disadvantages of high cost and health hazard as well as the agglomeration; although a new in-situ two-step sintering process can solve the above problems to some extent, yet the problems of low conversion ratio of the raw materials and the abnormal grain growth exist in this process. In this paper, an in-situ one-step synthesis technology is proposed, which means the growth of whiskers or nanoparticles and the sintering of the compact can be accomplished by one time in furnace. A kind of Ti(C, N)-based ceramic cutting tool material synergistically toughened by TiB<sub>2</sub> particles and whiskers is fabricated with this new process. The phase compositions, relationships between microstructure and mechanical properties as well as the toughening mechanisms are analyzed by means of X-ray diffraction (XRD) and scanning electron microscopy (SEM). The composite which is sintered under a pressure of 32 MPa at a temperature of 1700 °C in vacuum holding for 60 min can get the optimal mechanical properties. Its flexural strength, fracture toughness and Vickers hardness are 540 MPa, 7.81 MPa • m<sup>1/2</sup> and 20.42 GPa, respectively. The composite has relatively high density, and the in-situ synthesized TiB<sub>2</sub> whiskers have good surface integrity, which is beneficial for the improvement of the fracture toughness. It is concluded that the main toughening mechanisms of the present composite are whiskers pulling-out and crack deflection induced by whiskers, crack bridging by whiskers/particles and multi-scale particles synergistically toughening. This study proposes an in-situ one-step synthesis technology which can be well used for fabricating particles and whiskers synergistically toughened ceramic tool materials.

**Keywords:** in-situ synthesis technology, TiB<sub>2</sub> whisker; toughening mechanism, Ti(C, N)-TiB<sub>2</sub> composite, tool material

### 1 Introduction

Ceramic cutting tool materials have great advantages in the field of high-speed machining compared to the traditional high-speed steel and cemented carbide cutting tools, due to the high hardness, excellent wear and corrosion resistance of ceramics as well as good chemical stability. However, the brittleness and poor damage tolerance have limited the wide application of ceramics. Up to now, several useful methods have been proposed in order to improve the fracture toughness and flexural strength of ceramic materials, such as micro/nano-scale particles strengthening and toughening method<sup>[1]</sup>, whiskers/fibers/nanotubes or plate-like grains toughening method<sup>[2-5]</sup>, phase transformation toughening process and self-toughening technology<sup>[6]</sup>.

By separately adding nano-scale particles or whiskers with high strength and high elastic modulus into the ceramic matrix, the strength and toughness can be greatly improved<sup>[7-9]</sup>, especially when adding whiskers the high temperature mechanical properties of ceramics can be higher<sup>[10]</sup>. The strengthening and toughening effects get remarkable with the increased content of reinforcing phase; however, when the content of nano-scale particles is high, the nano-particles tend to agglomerate, thus during the sintering process, the agglomerate particles grow fast and develop into large grains, and the fast moving grain boundaries lead to mass of pores entrapped into the grown grains, which results in poor densification and is harmful to mechanical properties<sup>[1]</sup>. Similarly, when the whisker content is higher, whiskers are hard to be dispersed, and it is easier to form three dimensional rigid network skeletons, this skeleton structure can produce bridging and springing effects during sintering, leading to the poor density and mechanical properties<sup>[11]</sup>. Compared with separately adding particles or whiskers, simultaneously adding both particles and whiskers can weaken the agglomeration phenomenon to some extent, thus the unique strengthening and

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toughening effects of nano-scale particles and whiskers can be well developed, and the mechanical properties of ceramic cutting tool materials can be improved<sup>[12-14]</sup>. But the process of adding whiskers or nanoparticles still has the disadvantages of high cost and health hazard because of the flexible preparation process of whiskers with small production<sup>[11, 15]</sup>. In-situ synthesis technology can be used to directly fabricate reinforcing whiskers or particles in ceramic<sup>[2, 16]</sup> or metal matrix<sup>[17-19]</sup> and can be seen as an alternative strategy to overcome the above disadvantages. However, there are few reports about the in-situ synthesis of particles and whiskers toughened ceramic tool materials<sup>[20-22]</sup>.

Although the in-situ two-step sintering process (i.e., first step for fabricating whiskers or nanoparticles in matrix and the second step for sintering the compact)<sup>[20-21]</sup> can solve the above problems to some extent, yet the problems of low conversion ratio of the raw materials and the abnormal grain growth exist in this process. In the present work, an in-situ one-step synthesis technology is proposed, which means the growth of whiskers or nanoparticles and the sintering of the compact can be accomplished by one time in furnace. With this process, an in-situ TiB<sub>2</sub> particle-whisker toughened Ti(C, N)-TiB<sub>2</sub> ceramic cutting tool material was fabricated. The morphology and toughening mechanisms of whiskers were discussed.

## 2 Experimental Procedures

### 2.1 Precursor materials and preparation procedures

Commercially available Ti, B<sub>4</sub>C, BN and Ni powders were used as the precursor materials, of which Ni only acts as a sintering additive. The purity, particle size, manufacture and the main impurities of the precursor powders were shown in Table 1. The molar ratio of the precursor materials were listed in Table 2.

**Table 1. Purity, particle size, manufacture and impurity of the precursor materials**

Substance	Purity wt. %	Particle size <i>d</i> /μm	Manufacture	Main impurity and comment wt. %
Ti	~99.0	~48	GRINM, China	CaO<0.05, MgO<0.05, SiO <sub>2</sub> <0.01, TiO <sub>2</sub> <0.005, Fe <sub>2</sub> O <sub>3</sub> <0.005
BN	~99.0	~1	YPFC, China	B <sub>2</sub> O <sub>3</sub> >0.28, N <sub>3</sub> Na>0.14, CaO>0.02, Fe <sub>2</sub> O <sub>3</sub> >0.05, Al <sub>2</sub> O <sub>3</sub> >0.006
B <sub>4</sub> C	~99.5	~1	YPFC, China	Fe<0.05, Si<.05, C<0.5, O<0.3
Ni	~99.8	~48	GRINM, China	Co<0.05, C<0.03, Fe<0.03, Pb<0.003, S<0.003, Mg<0.002

**Table 2. Mol ratio of the precursor materials**

Samples No.	Mol ratio of the precursor materials α/mol. %		
	Ti	BN	B <sub>4</sub> C
TBCN	2.9	0.7	0.3

The mixed slurries were ball-milled, and then dried in a vacuum dry-type evaporator (Moder ZK-82A, China). After that, the dried powders were sieved through a 100-mesh sieve for further use. The dried powders were placed into a graphite die and in-situ hot-pressed with an applied pressure of 32 MPa at 1700°C with the holding time of 60 min in vacuum in a sintering furnace.

### 2.2 Characterization

The sintered compacts were cut, ground and polished into specimens with a dimension of 3 mm×4 mm×30 mm. The flexural strength was tested using the three-point bending tester (Model WD-10, China) with a span of 20 mm and a loading velocity of 0.5 mm/min. The Vickers hardness was measured on the polished surface using a Vickers diamond pyramid indenter (Model 120, China) with a load of 196 N and a loading holding time of 15 s. The fracture toughness measurement of materials was determined by the Vickers indentation method proposed by EVANS, et al<sup>[23]</sup>. The relative density of specimens was measured by the Archimedes' method with the distilled water as medium. The fractured surfaces and cracks on the polished surfaces were observed by scanning electron microscopy (SEM, SUPRA-55, ZEISS, Germany). Phase identification was carried out by X-ray diffraction analysis (XRD, RAX-10A-X, Hitachi, Japan) with copper Kα radiation.

## 3 Results and Discussion

### 3.1 Phase composition and microstructure

Fig. 1 showed the XRD pattern of the sample. It revealed that TiC<sub>0.3</sub>N<sub>0.7</sub> and TiB<sub>2</sub> were the major phases synthesized by reaction (1) in the sintering process, and there were no other intermediate phases or impurities.

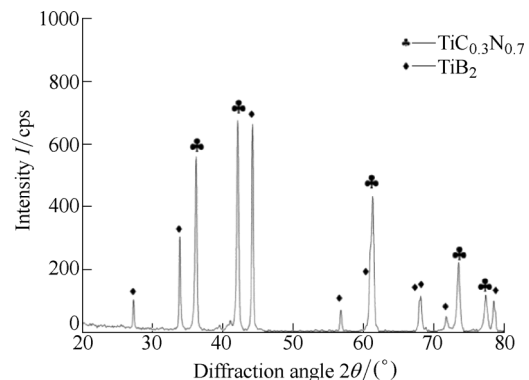
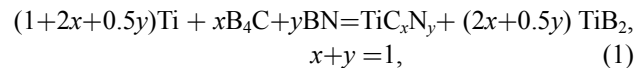
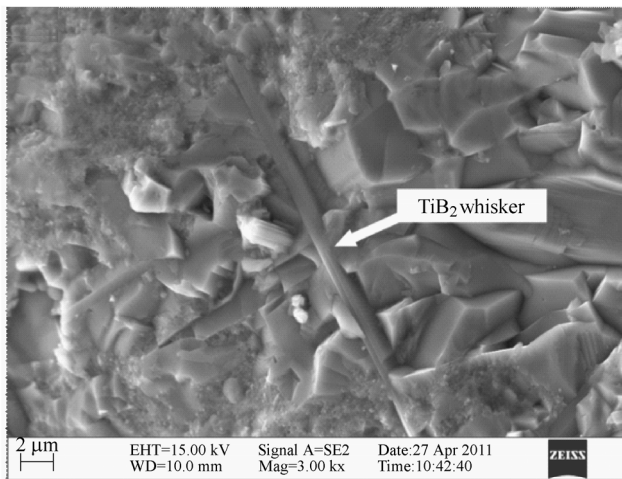
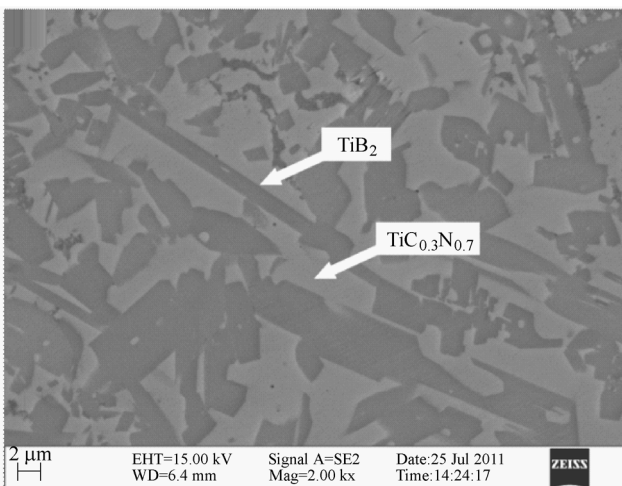


Fig. 1. XRD pattern of Ti(C,N)-TiB<sub>2</sub> ceramic tool material

The SEM morphology of fractured surface of the sintered composite was shown in Fig. 2(a). It revealed that the diameter, length and aspect ratio of TiB<sub>2</sub> whiskers were about 0.5–1 μm, 20 μm and 20, respectively. The TiB<sub>2</sub> whiskers synthesized by in-situ reaction had complete and clean surface, and the whisker section presented regular hexagon or quadrangle. Fig. 2(b) showed the SEM morphology of polished surface of the composite. The black phase was TiB<sub>2</sub> and the grey phase was TiC<sub>0.3</sub>N<sub>0.7</sub>. It was found that the whiskers are uniformly distributed among the matrix, and the pores were hardly observed on the polished surface, which indicated that the composite had high density. Therefore, the integrated fabrication process of whisker synthesis and composite densification was achieved by one step.



(a) Fractured surface



(b) Polished surface

Fig. 2. SEM morphology of fractured surface and polished surface of Ti(C, N)-TiB<sub>2</sub> composite

### 3.2 Mechanical properties and toughening mechanisms

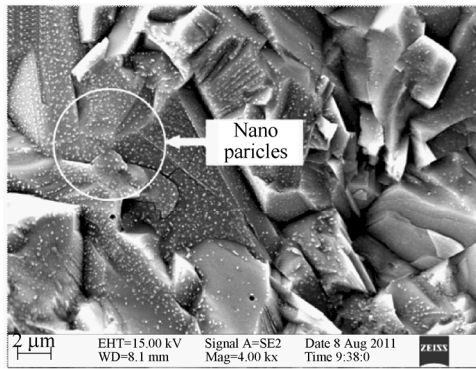
The mechanical properties of the sintered composite

ceramic tool material were shown in Table 3. The fracture toughness of the whisker-toughened composite synthesized by in-situ reaction was improved markedly. Due to the high elasticity modulus and high strength of TiB<sub>2</sub> whiskers, when the external load was applied on the material, the TiB<sub>2</sub> whiskers could well undertake and transfer the load, thus the flexural strength of the composite was enhanced. Additionally, instant high temperature induced by the exothermic reaction (1) promoted the densification, leading to the higher density, which is beneficial for the increase of flexural strength.

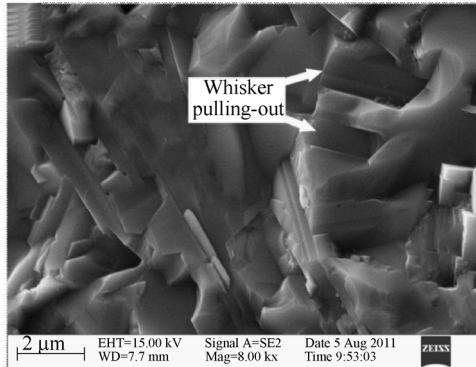
**Table 3. Mechanical properties of Ti(C, N)-TiB<sub>2</sub> composite ceramic tool material**

Composite	Flexural strength $\sigma_f$ /MPa	Vickers hardness $H_V$ /GPa	Fracture toughness $K_{1C}$ /(MPa · m <sup>1/2</sup> )
Ti(C,N)-TiB <sub>2</sub>	540	20.42	7.81

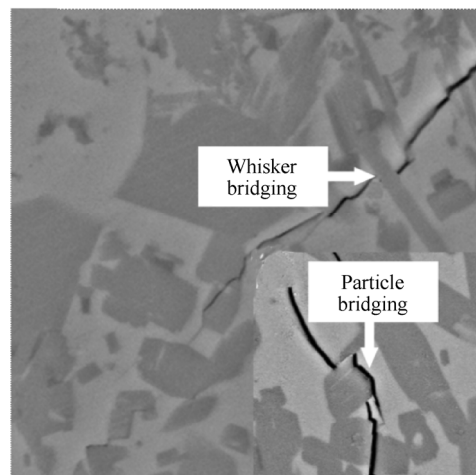
The fracture toughness of the composite was much higher than that of monolithic Ti(C, N) or TiB<sub>2</sub>. The increased fracture toughness was ascribed to the synergistic toughening effects of the in-situ synthesized whiskers and particles. The main toughening mechanisms were analyzed combining with the SEM morphologies shown in Fig. 3(a) to Fig. 3(e). Firstly, the nano-scale phases formed from the in-situ reaction were uniformly distributed at the surfaces of whiskers and particles, which made the interfaces much coarser as shown in Fig. 3(a). Thus, it was believed that the coarse surface could enhance the frictional force when whiskers pulling-out from the matrix. Secondly, Fig. 3(b) showed the left holes after the whiskers pulling-out. Whisker pulling-out would consume much more fracture energy, so the fracture toughness would be promoted. Moreover, the effects of whiskers pulling-out could relax the stress of crack tip, and then the stress intensity factor of crack tip reduced. So, the effects of whisker pulling-out were beneficial for the increase of fracture toughness. Thirdly, cracks were bridged by a portion of TiB<sub>2</sub> whiskers and particles located at particular places as shown in Fig. 3(c) and Fig. 3(d). The crack bridging whiskers and particles connect two surfaces of a crack and provide with a force which makes two surfaces of a crack draw close. This results in the increase of stress strength factor of the composite with the extension of crack. Fourthly, Crack deflection was also observed in Fig. 3(e). Due to the high strength of TiB<sub>2</sub> whisker, when the cracks encounter TiB<sub>2</sub> whisker, the cracks tended to be deflected and propagated along the TiB<sub>2</sub> whisker. Thus the crack propagation path extended, which was beneficial for improving the toughness by the increased consumption of fracture energy. Moreover, the particle size ranging from nano-scale to micro-scale had the multi-scale synergistically strengthening and toughening effects.



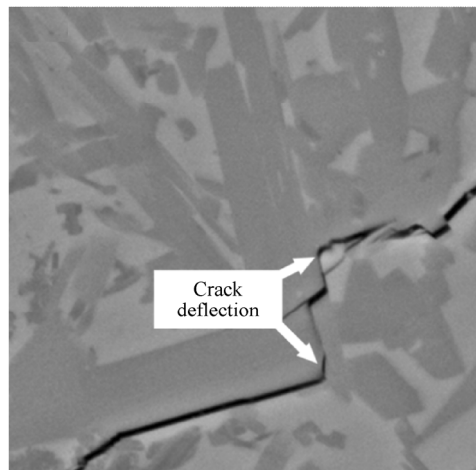
(a) Nano-scale particle toughening



(b) Whisker pulling-out



(c) Whisker bridging, (d) Particle bridging



(e) Crack deflection

Fig. 3. SEM morphology showing different toughening mechanisms

## 4 Conclusions

(1) A type of Ti(C, N)-based ceramic cutting tool material synergistically toughened by  $\text{TiB}_2$  particles and whiskers was fabricated by in-situ synthesis technology, with this process the whisker synthesis and composite densification were carried out by one step. The composite had relatively high density, and the  $\text{TiB}_2$  whiskers possessed good surface integrity.

(2) The fracture toughness of the new Ti(C, N)- $\text{TiB}_2$  composite was markedly improved up to  $7.81 \text{ MPa} \cdot \text{m}^{1/2}$ . The flexural strength and Vickers hardness were 540 MPa and 20.42 GPa, respectively.

(3) The main toughening mechanisms of the present composite were crack bridging by whiskers and particles, whiskers pulling-out, crack deflection and multi-scale particles synergistically toughening.

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